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Article

Effect of Time-Real Marine Environment Exposure on the Mechanical Behavior of FRP Composites

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Abstract: Fiber reinforced polymer (FRP) composites coupons were exposed to real sea environment to assess the influence on the mechanical behavior of composite materials used in the construction of marine structures. Real-life sea environment conditions were opted for instead of the more common simulated and laboratory versions of seawater in the attempt to obtain more realistic structural modeling environmental input design parameters for marine structures. Exposure was performed over prolonged time span instead of the usual accelerated tests. Epoxy and polyester resins, reinforced with glass fibers in three fiber layout configurations, were used to manufacture standardized tensile testing coupons. Mass changes due to seawater absorption, microorganism growth, changes in tensile strength (standard tensile tests), and surface morphology of the coupons were evaluated after 6- and 12-month long periods of submersion in the sea in the Rijeka bay, Croatia. All specimens showed mass increase due to water absorption and growth of attached algae and sea microorganisms. Various levels of reduction in tensile strength, depending on the fiber layout configurations, were observed. Significant changes in the matrix material structure were noticed, effectively producing “voids”. Based on these results, sustainability of FRP composites in marine environment is addressed and discussed.

Keywords: composites; sustainability of composites; marine environment; FRP composites



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1. Introduction

Fiber reinforced polymer (FRP) composites were used in the construction of marine vessels and structures since the middle of the 20th century, whether it be as an exclusive option for construction [1] or as a combination with traditional materials, such as steel [2] or concrete [3]. The design of these structures in aspects of strength, durability, and environmental influence on the mechanical properties was based mainly on experience for the best part of the said period. In the last couple of decades, significant effort was made to combine the experimental and scientific knowledge obtained so far in these field of research to enable prediction models that can be safely used to achieve sustainable and safe design of marine structures [4–7].

Mechanical properties of composite materials can be customized accordingly to specific applications demands by defining layup sequences, number of plies, and fiber orientation in the load direction [8–10], which makes them appealing for design of marine structures with complex shapes. As the application field for marine composites widens, the request for resilience to mechanical loading and environmental influences rises. Adequate knowledge of limit state assessment, durability and life span, failure modes, fracture toughness, fire resistance, and environment influence parameters are crucial for an efficient and sustainable design process for structures in this demanding industry sector [11].

The micromechanical aspect of composite materials design is often considered too complex and time-consuming for marine structural designers to deal with. The scientific

research in this field of study should be aimed at simplifying the complex micromechanical level analysis and transform it into simple-to-use and time-saving engineering tools. The current practice for obtaining data for composites failure is based on experiments. As experiments can be relatively expensive and microscale data are usually unavailable to shipbuilders, they often turn to data and models prescribed by rules and procedures, thus leading to empirical based design process of marine structures. All of this yields rules that are very conservative in formulating design requests, which in turn hinders optimal design of marine structures concerning failure mechanisms.

One of the most important parameters influencing the mechanical properties of composite materials in marine applications is the absorption of seawater [12]. Previous research on this matter is based on immersing test samples, called coupons, in laboratory conditions using accelerated procedures [13] to simulate 20+ years of expected lifespan of typical marine structures [14,15]. The ageing of composites is usually carried out in climatic chambers in laboratory conditions [6,16,17] to reduce the time of the test [18–21].

In addition, water absorption tests are often done with tap water, demineralized water, or artificial seawater [22,23]. This approach yields a lack of long-term data pertaining to degradation of mechanical properties exposed to the marine environment. Furthermore, the effects of the moving seawater (waves, sea level variations due to tides) and radically variant environmental effects that a typical marine vessel or structure are exposed to during their life cycle (vessels sailing all over the world, changes in salinity, climate) are not considered in accelerated ageing laboratory methods.

The absorption process of moisture and water of a composite exhibits complex behavior and dependence on various factors [24], such as resin type and curing characteristics, void content, resin/fiber volume fractions [25], the manufacturing technique, etc., [26–28].

All this served as motivation to concentrate the research presented here on the influence of absorbed water on marine composites in real-life conditions, not laboratory, by submerging the coupons in the sea for prolonged periods of 6 and 12 months.

The dominant choice of composite materials in the civil sector of the marine vessels industries is glass fiber reinforced plastics (GRP), both for commercial and leisure vessels hulls [29], resulting in a more cost-effective product. Classification societies can be somewhat restrictive when it comes to allowing composites as structural material. The choice of fibers is restricted to E-glass or carbon fibers, whilst resins are limited to epoxy, polyester, or vinyl-ester [30–32].

The scope of the experimental research presented in this paper is the absorption of composite coupons in real sea environment and the assessment on the impact of the seawater on the mechanical properties of the material.

2. Materials and Methods

2.1. Materials

The ISO 527-4 [33] standard prescribes the testing procedures for determination of tensile properties of fiber-reinforced plastic composites, both for unidirectional (UD) and multidirectional reinforcements.

In this paper, epoxy and polyester resins with glass fibers were used to manufacture standardized tensile testing coupons. Two matrix/fiber combinations were used, namely epoxy/glass and polyester/glass. The epoxy resin (Sicom SR 8200 and SD 720 series hardener) and the polyester resin (Reichhold POLYLITE 507-574) mechanical properties are shown in Table 1, as provided by the manufacturers of each component.

Table 1. Resin systems properties.

Property	Epoxy	Polyester
Tensile strength [MPa]	47	42
Elasticity modulus [MPa]	3240	2700
Glass transition temperature [°C]	50	55

The fibers used in manufacturing the coupons are in the form of a UD stitched E-glass fiber fabric (Sicomun UDV600), with 594 g/m² ply specific area weight.

Four different layup configurations were chosen for both matrix/fiber combinations to evaluate mechanical properties deterioration in the marine environment. The layup schematics are as follows, according to standard notation for composite layup [34]:

- Unidirectional with longitudinal fiber orientation—UD0
- Multidirectional—(0/90)s
- Multidirectional—(0/45/90)s.

Three rectangular plates measuring 300 × 450 mm with three different layup schemes UD0, 0/90, (0/45/90), were produced for each of the material combinations using 8 plies of the UD fabric per plate, Figure 1. The epoxy/glass plates were produced by vacuum assisted infusion process, resulting in 3 ± 0.2 mm thick plates. The infusion process proved problematic for the polyester resin as it was resulting in dry fibers on the tool surfaces, so the polyester/glass plates were finally produced by hand layup process, resulting in 5 ± 0.5 mm thick plates.

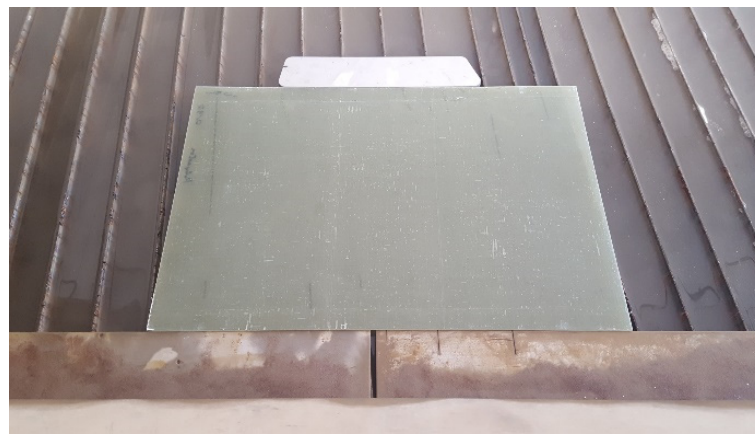


Figure 1. Composite plate prepared for waterjet cutting.

2.2. Coupons and Exposure to Marine Environment

Coupons measuring 250 mm in length and 25 mm in width [33] were then cut out of the plates on a waterjet cutting machine (OMAX Maxiém series), Figure 2. The cutting pressure was between 1400 and 3400 bar, with the average cutting speed of 1187 mm/min.

Waterjet cutting was chosen based on previous experience in cutting similar materials. The brittleness of glass and composite materials causes localized damage on the locations of first contact of the cutting high-pressure waterjet with the material. This enabled the precise positioning of the damage point on the coupon gauge length during the configuration of the waterjet machine. The intent here is to introduce a damage point, which is to simulate real damage on marine structures. This damage point represents a facilitated entry point of seawater in a real structure. Composite marine vessels and structures are usually protected by a final layer of gel coat that protects them from water penetration. When this protective layer is damaged during application, a more significant sea water intake rate in the structure material is enabled.

All the coupons were then weighed dry and measured with a ±0.1 mm accuracy.

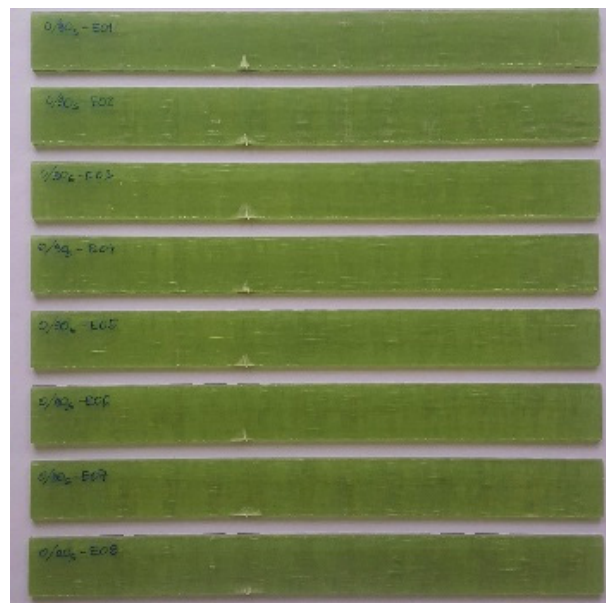


Figure 2. Cut-out coupons.

The machined coupons were divided into 2 main groups by material combinations (epoxy/glass, polyester/glass), and in 3 subgroups according to the duration of exposure to the marine environment (dry, 6 months, 12 months). Each group consisted of 5 specimens (coupons); the first subgroup of coupons was not submerged but tested dry, to be used as a control group.

The other two subgroups were exposed to real-life sea environment, i.e., submerged into the sea on a depth of 10 m, at northern Adriatic in front of the city of Rijeka in Croatia for a duration of 6 and 12 months, respectively. The sea temperature at the location of experiment varies between 10–14 °C annually, salinity changes between 37.8–38.3 PPT, while the pH value is between 8.22–8.29 [35]. The coupons were mounted on special stainless-steel frames (AISI 316L), shown in Figure 3.

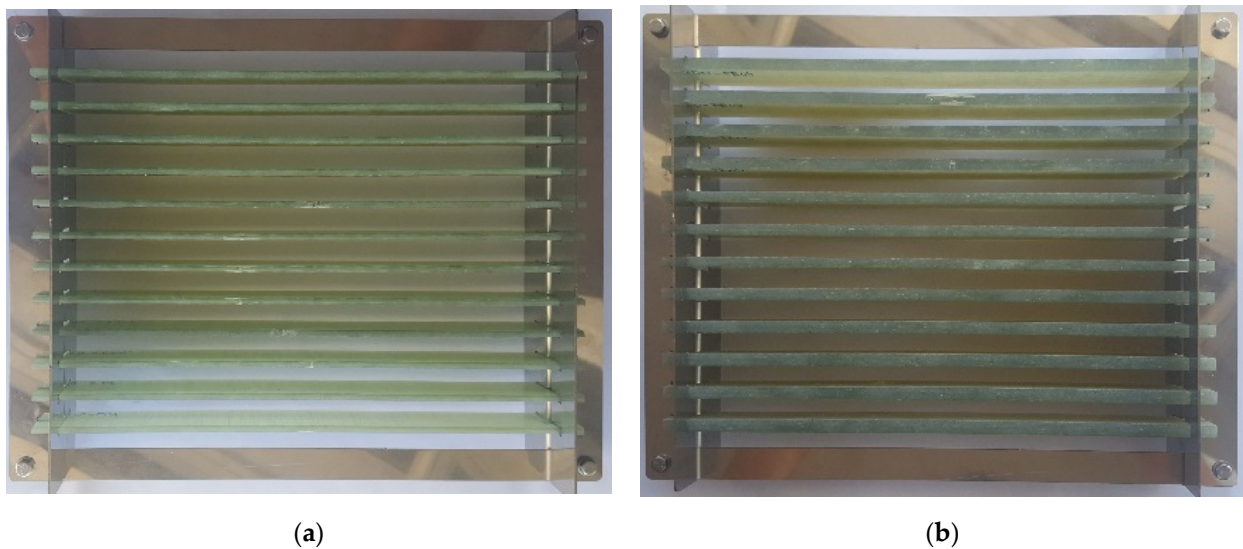


Figure 3. Coupons mounted on special stainless-steel frame before submersion: (a) epoxy/glass; (b) polyester/glass.

2.3. Testing Procedures

Each coupon was weighed with the same digital scale with a 200 g measuring range and 0.01 g resolution before (dry) and after the submerging time-period to determine the mass gain of the absorbed seawater. Wet coupons were taken out of the sea, cleaned from sea organisms accumulated during submersion with a soft brush, still submerged in seawater. Special care was taken not to damage the coupon. After cleaning, the coupons were left to drain, dried superficially with a cloth, and weighed all under one minute to assure minimal possible drying of the coupons.

Reinforcement tabs, made of printed circuit board cutouts, were added at the coupon ends before the tensile test to minimize the influence of the grips pressure on the test results [36]. The size of the tabs was chosen based on ISO 527-4 recommendations, Figure 4.

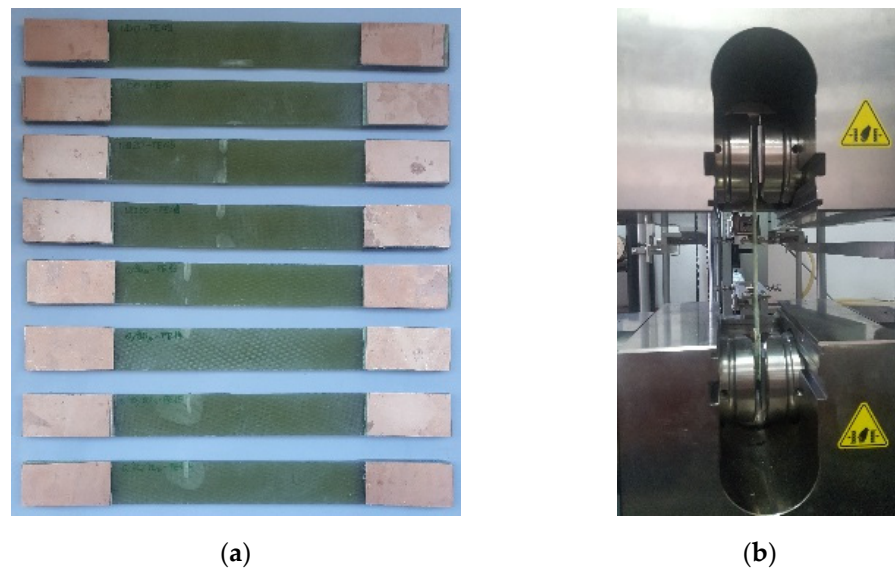


Figure 4. Coupons: (a) with reinforcement tabs; (b) gripped in tensile testing machine.

Uniaxial tensile tests used for the determination of the material properties were performed on a Zwick 400 kN (ZwickRoell GmbH, Germany) universal testing machine. A macro extensometer was used to measure the specimens' elongation. The displacement rate of the testing machine crosshead during testing was 2 mm/min.

Tensile testing was conducted in accordance with ISO 527 series standards recommendations.

Microscopical investigation was performed on fractured coupons of three fiber layout configurations (UD0°, (0/90)s, (0/45/90)s) and for both dry coupons and coupons submerged in the sea for different periods i.e., 6 and 12 months. Surface and cross-sectional images were taken of all coupons, with special attention given to the grips areas (A) and locations with observed damage after the tensile test (B), Figure 5.

Optical microscopy systems (Olympus SZX10 stereo optical microscope and Olympus BX51 SM optical microscope analysis system, both produced by Olympus corporation, Japan) and scanning electron microscope (SEM, FEI QUANTA 250 FEG, FEI Company, USA) with the OXFORD INSTRUMENTS PENTAFET, UK, Energy Dispersive Spectroscopy (EDS) analysis module were used to investigate the state of the coupon's surfaces exposed to real sea environment and to identify changes in surface morphology caused by the exposure to seawater. Photographs were taken before and after the tensile tests.

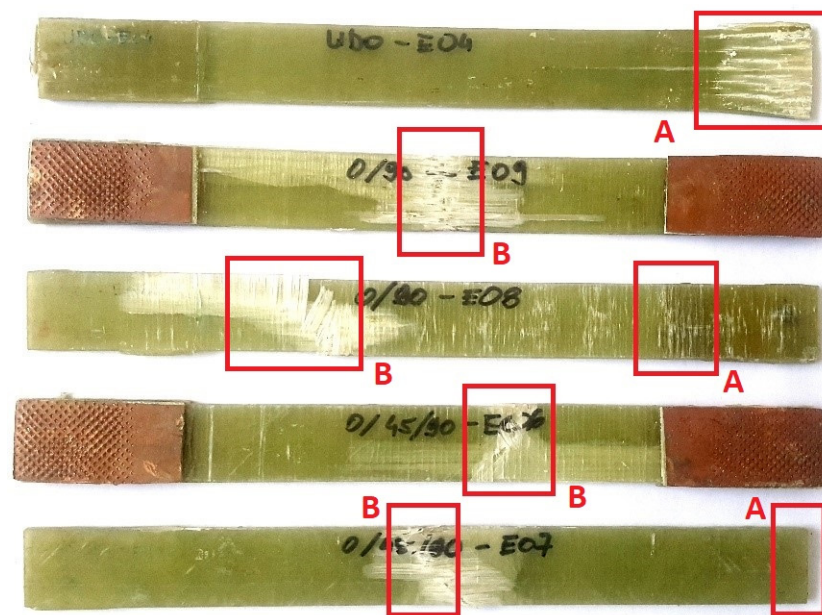


Figure 5. Coupons after tensile testing; locations for microscopical examination.

3. Results

The results of the experimental investigation of epoxy/glass and polyester/glass coupons exposed to marine environment are presented in the form of diagrams, images, and tables. Experimental testing results shown here are comprised of coupon weight change (seawater absorption, algae growth) analysis, tensile strength determination, and surface morphology changes observations.

3.1. Algae and Marine Organisms Growth

The average aggregate mass gain due to the coupled algae/marine organisms' growth and water absorption for the two matrix resins is given in Table 2.

Table 2. Mass gain due to algae growth and water absorption.

Resin	Period of Exposure	Mass Increase [%]		
		Minimum	Maximum	Average
Epoxy	6 months	0.929	3.892	1.971
	12 months	5.070	11.175	7.856
Polyester	6 months	0.863	1.758	1.286
	12 months	2.551	13.940	8.687

3.2. Water Absorption and Mass Change Analysis

The cleaned coupons' mass measurement results after the period of 6 and 12 months of submersion are shown below, Figure 6.

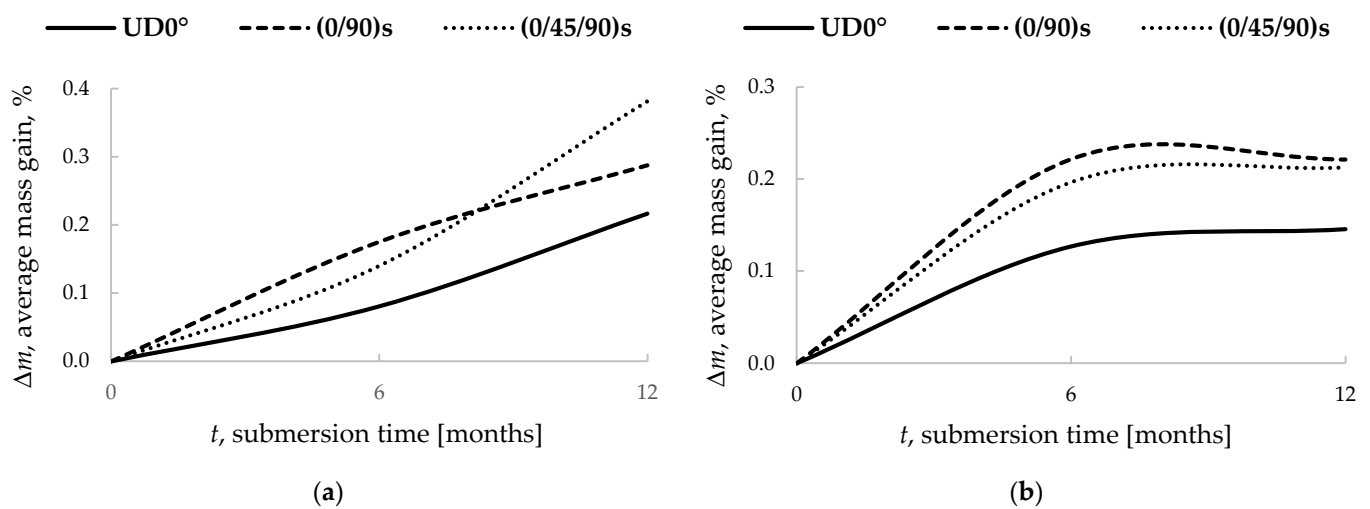


Figure 6. Average mass gain due to seawater absorption: (a) epoxy resin; (b) polyester resin.

The minimum and maximum values of the mass gain for all layout configurations and material combinations are given in Tables 3 and 4.

Table 3. Mass gain due to seawater absorption, epoxy resin.

Fiber Layout Configuration	Period of Exposure	Mass Increase [%]		
		Minimum	Maximum	Average
UD0°	6 months	0.070	0.092	0.081
	12 months	0.133	0.300	0.217
(0/90)s	6 months	0.158	0.211	0.175
	12 months	0.087	0.423	0.288
(0/45/90)s	6 months	0.078	0.198	0.140
	12 months	0.252	0.502	0.381

Table 4. Mass gain due to seawater absorption, polyester resin.

Fiber Layout Configuration	Period of Exposure	Mass Increase [%]		
		Minimum	Maximum	Average
UD0°	6 months	0.099	0.155	0.127
	12 months	0.018	0.199	0.103
(0/90)s	6 months	0.194	0.258	0.222
	12 months	0.040	0.128	0.083
(0/45/90)s	6 months	0.070	0.300	0.197
	12 months	0.173	0.266	0.213

3.3. Tensile Test Results

Engineering stress-strain diagrams were obtained from performed uniaxial tensile strength on dry coupons and wet coupons that were submerged in the sea for 6 and 12 months, Figures 7–12.

The change in tensile strength due to the prolonged submersion in seawater is shown in Figures 13 and 14.

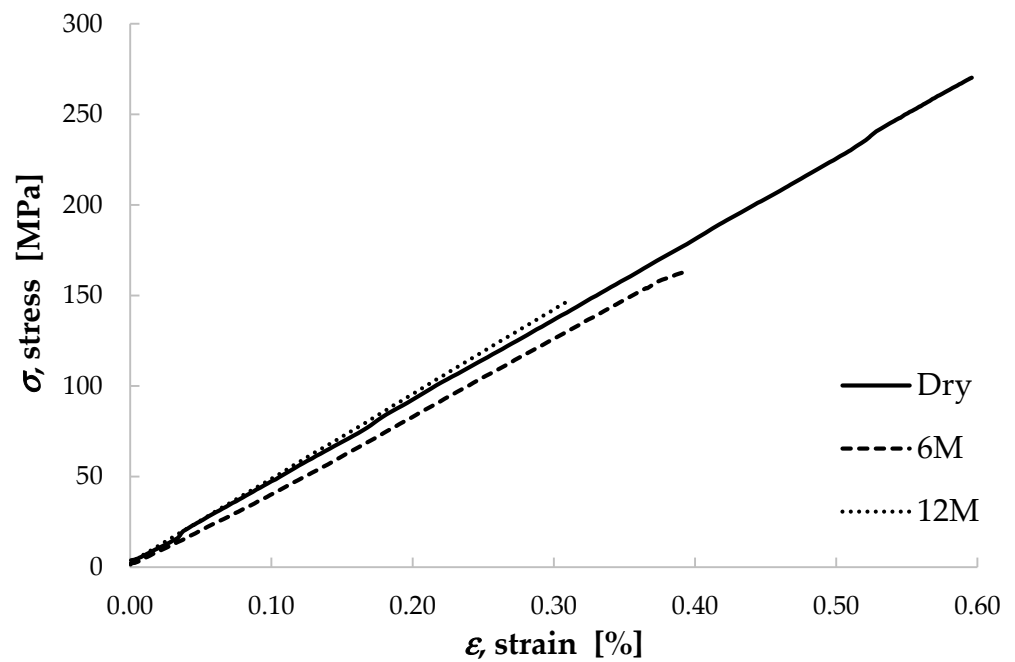


Figure 7. Engineering stress-strain diagrams for epoxy/glass UD0° coupons submerged in sea for 6 (6 M) and 12 months (12 M).

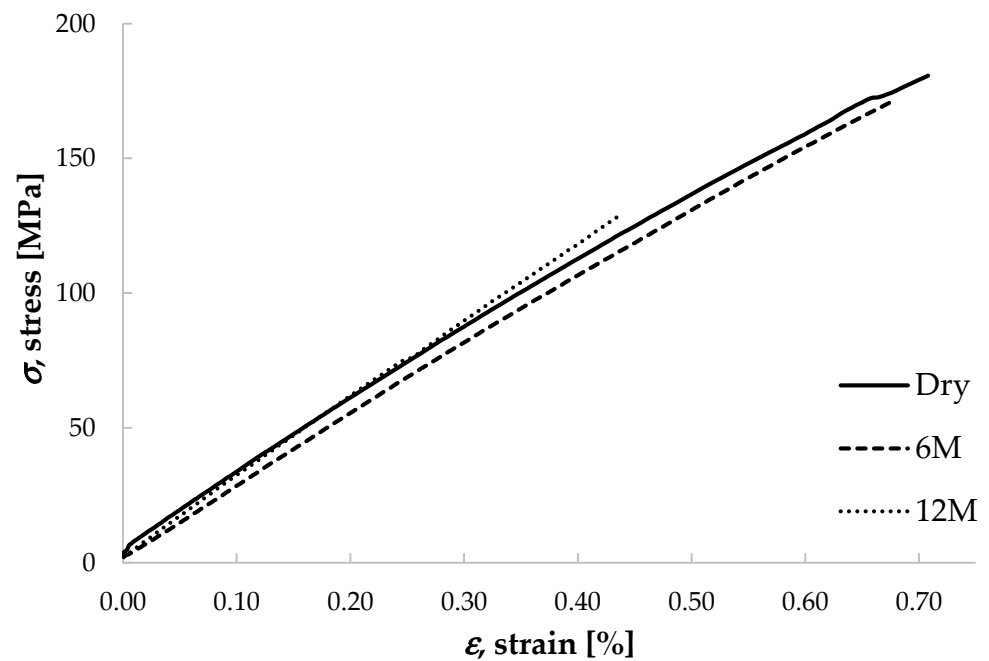


Figure 8. Engineering stress-strain diagrams for epoxy/glass (0/90)s coupons submerged in the sea for 6 (6 M) and 12 months (12 M).

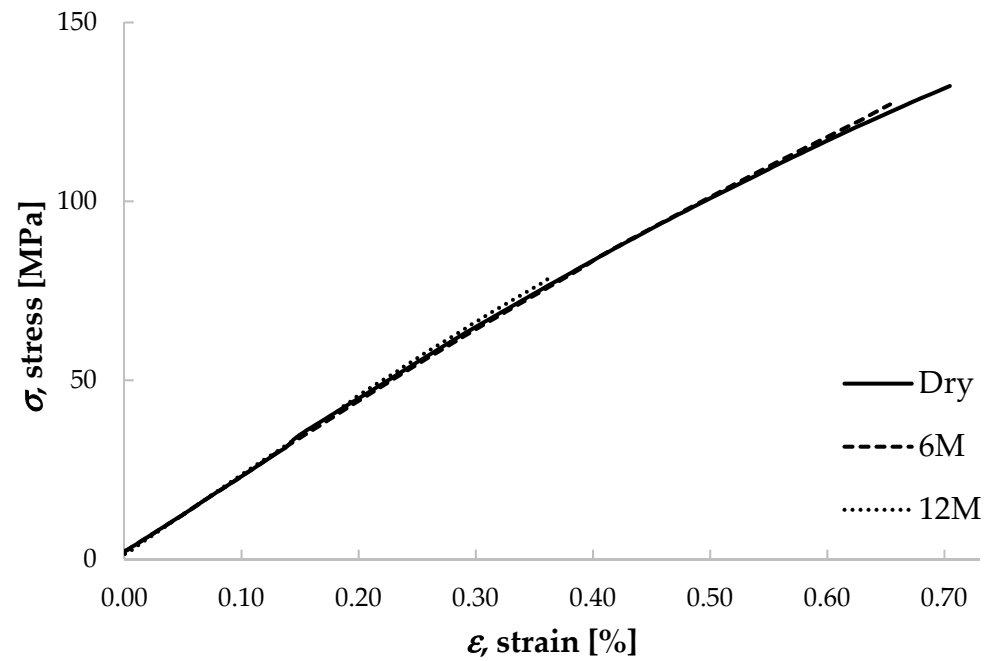


Figure 9. Engineering stress-strain diagrams for epoxy/glass (0/45/90)s coupons submerged in sea for 6 (6 M) and 12 months (12 M).

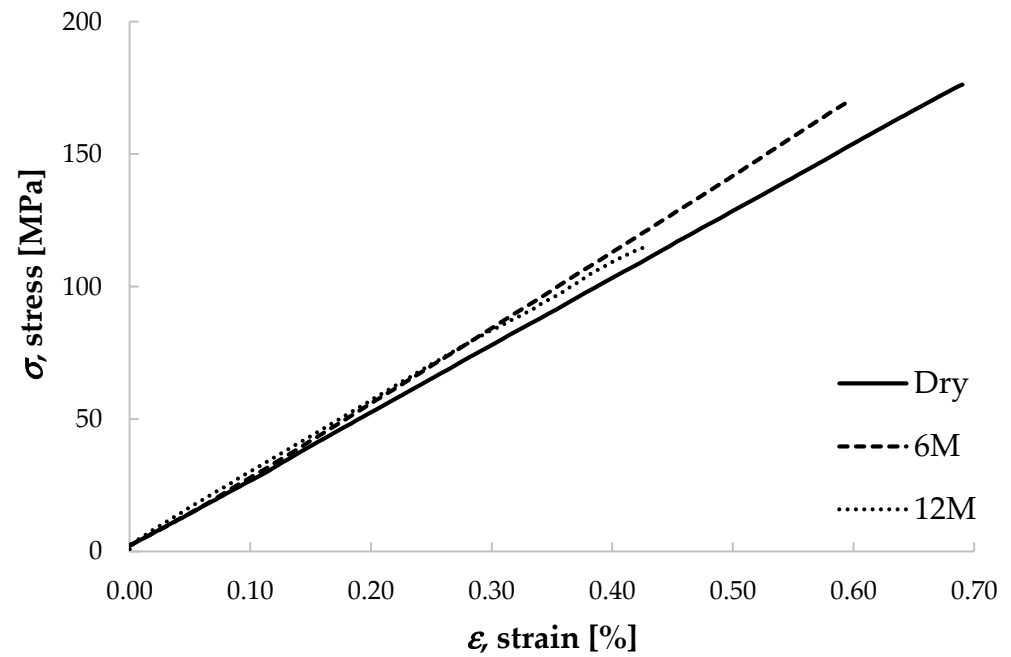


Figure 10. Engineering stress-strain diagrams for polyester/glass UD0° coupons submerged in sea for 6 (6 M) and 12 months (12 M).

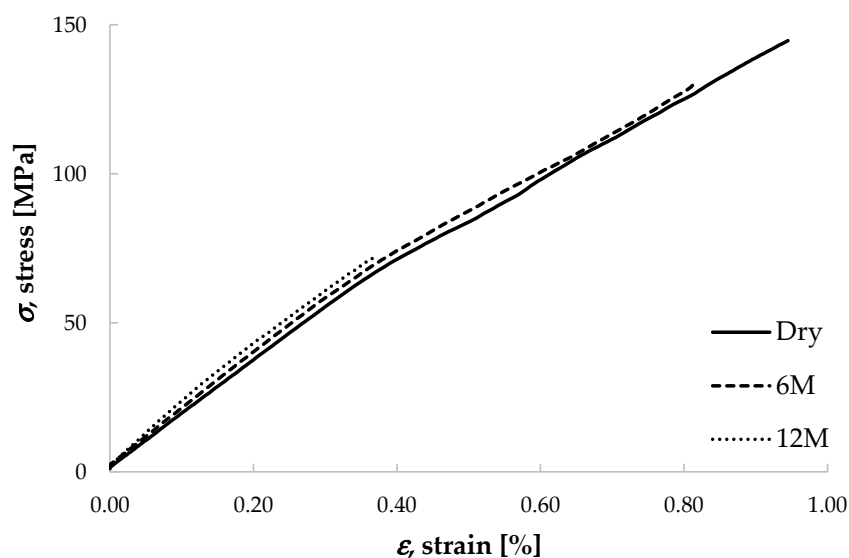


Figure 11. Engineering stress-strain diagrams for polyester /glass (0/90)s coupons submerged in sea for 6 (6 M) and 12 months (12 M).

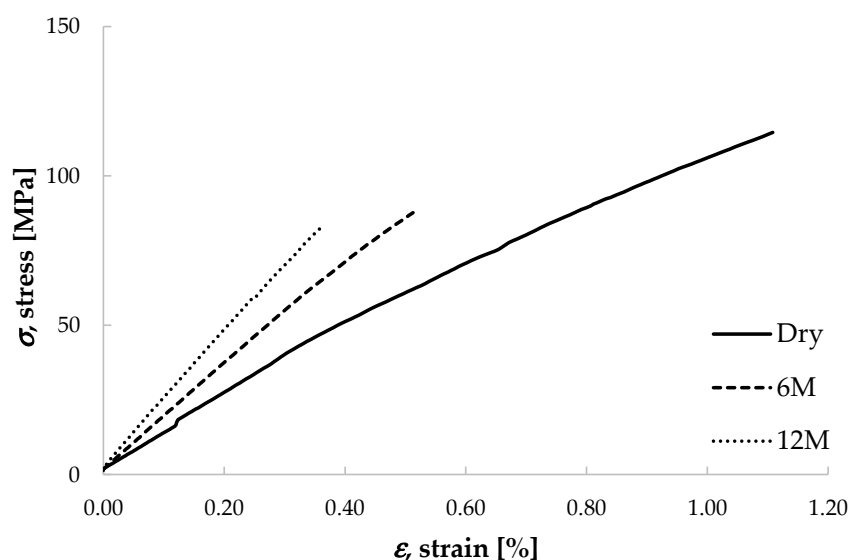


Figure 12. Engineering stress-strain diagrams for polyester /glass (0/45/90)s coupons submerged in sea for 6 (6 M) and 12 months (12 M).

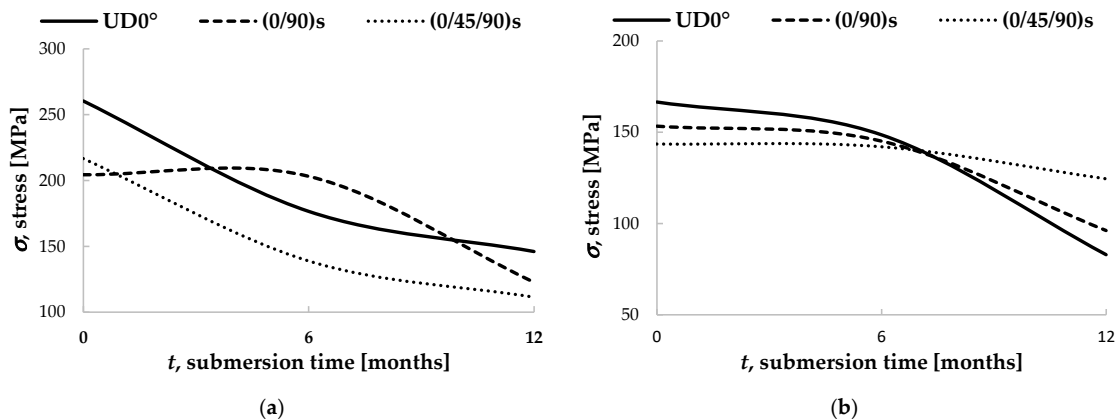


Figure 13. Average tensile strength degradation: (a) epoxy resin coupons; (b) polyester resin coupons.

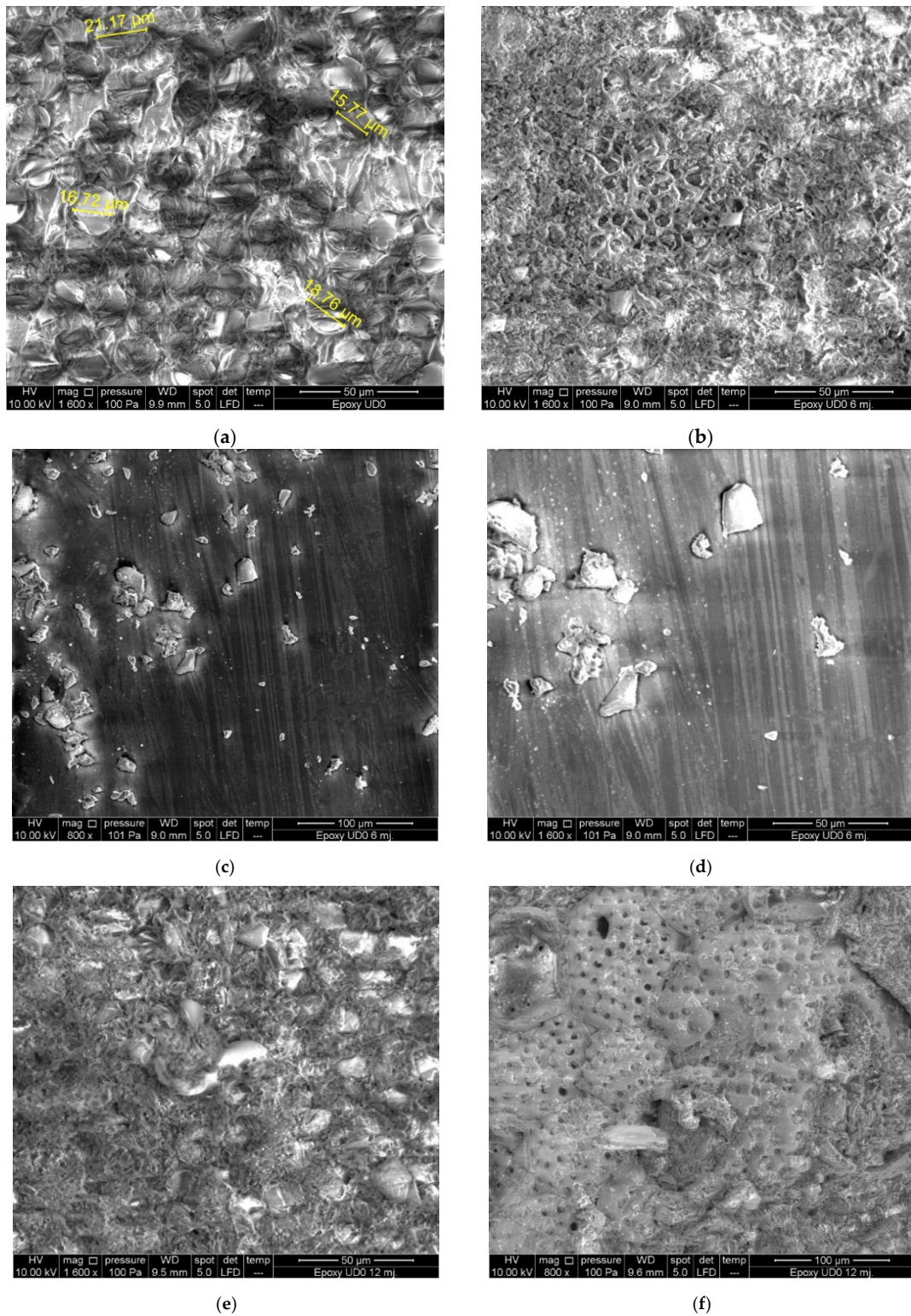


Figure 14. SEM epoxy UD0°: (a) dry; (b) 6 months submersion; (c,d) salt crystals after 6 months; (e,f) microorganisms' growth after 12 months.

3.4. Microscopical Investigation

Surface and cross-sectional images obtained by optical microscopy are not presented here but are available in a publicly accessible repository to save paper space and keep the readers focus on the more detailed and more illustrative SEM results.

The images obtained by SEM investigation are presented in Figures 14–19. Only some representative images were chosen as a portrayal of the performed research to limit the length of the paper, whilst the complete set of all obtained images is posted on an online repository as Supplementary Materials to this article.

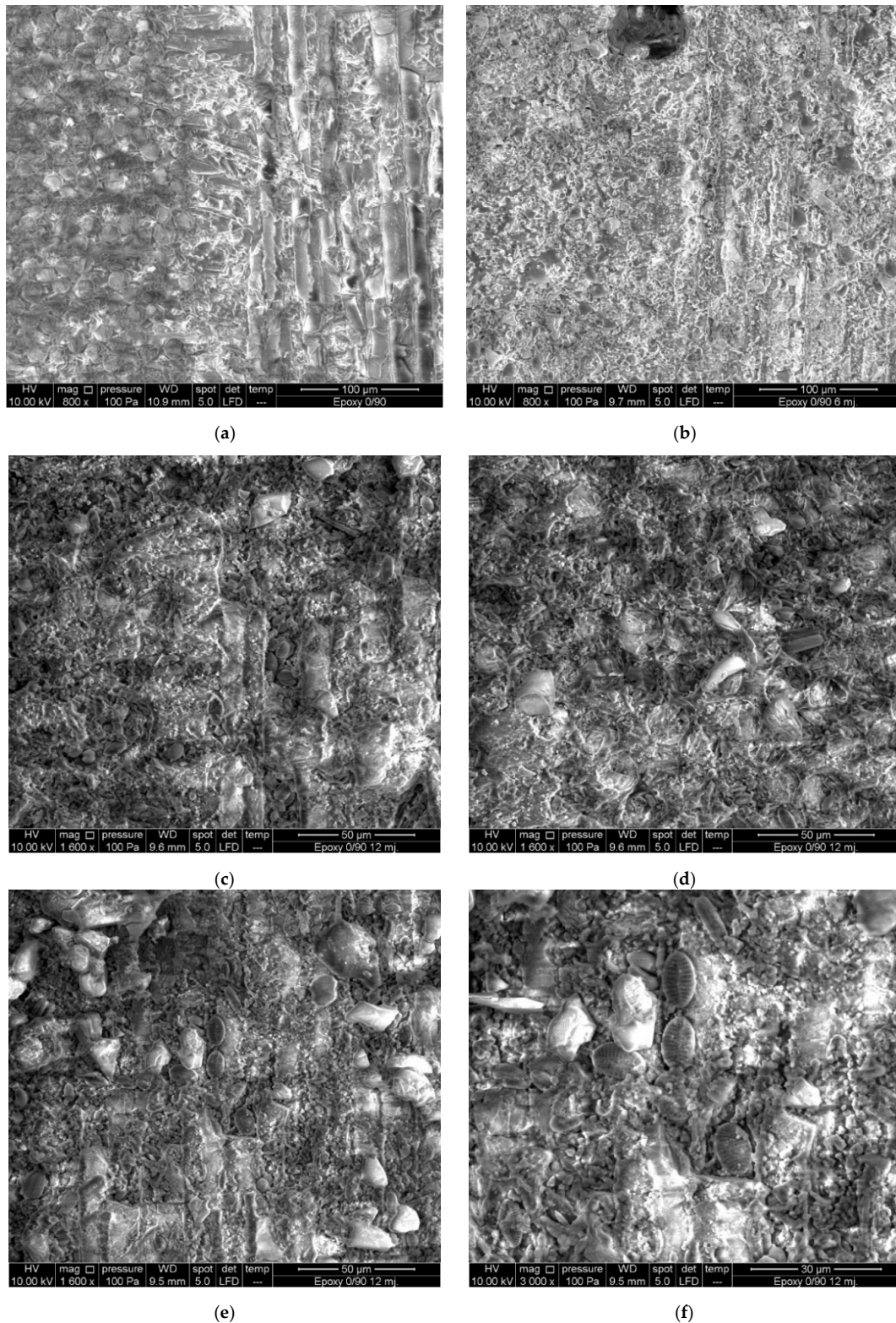


Figure 15. SEM epoxy (0/90): (a) dry; (b) 6 months submersion; (c,d) salt crystal formations; (e,f) microorganisms' growth after 12 months.

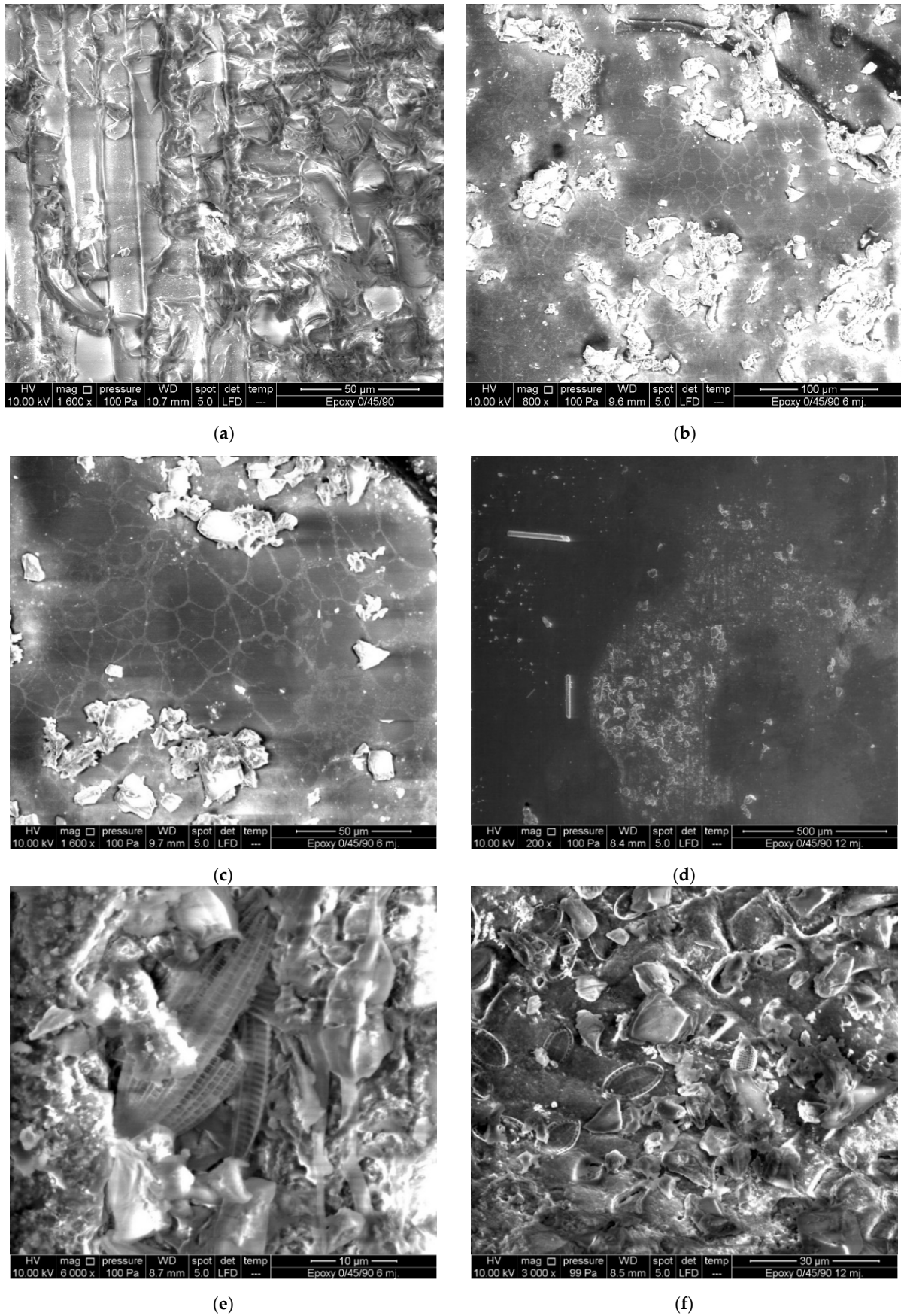


Figure 16. SEM epoxy (0/45/90)s: (a) dry; (b–d) salt crystals 6 and 12 months submersion; (e,f) microorganisms' growth after 6 and 12 months.

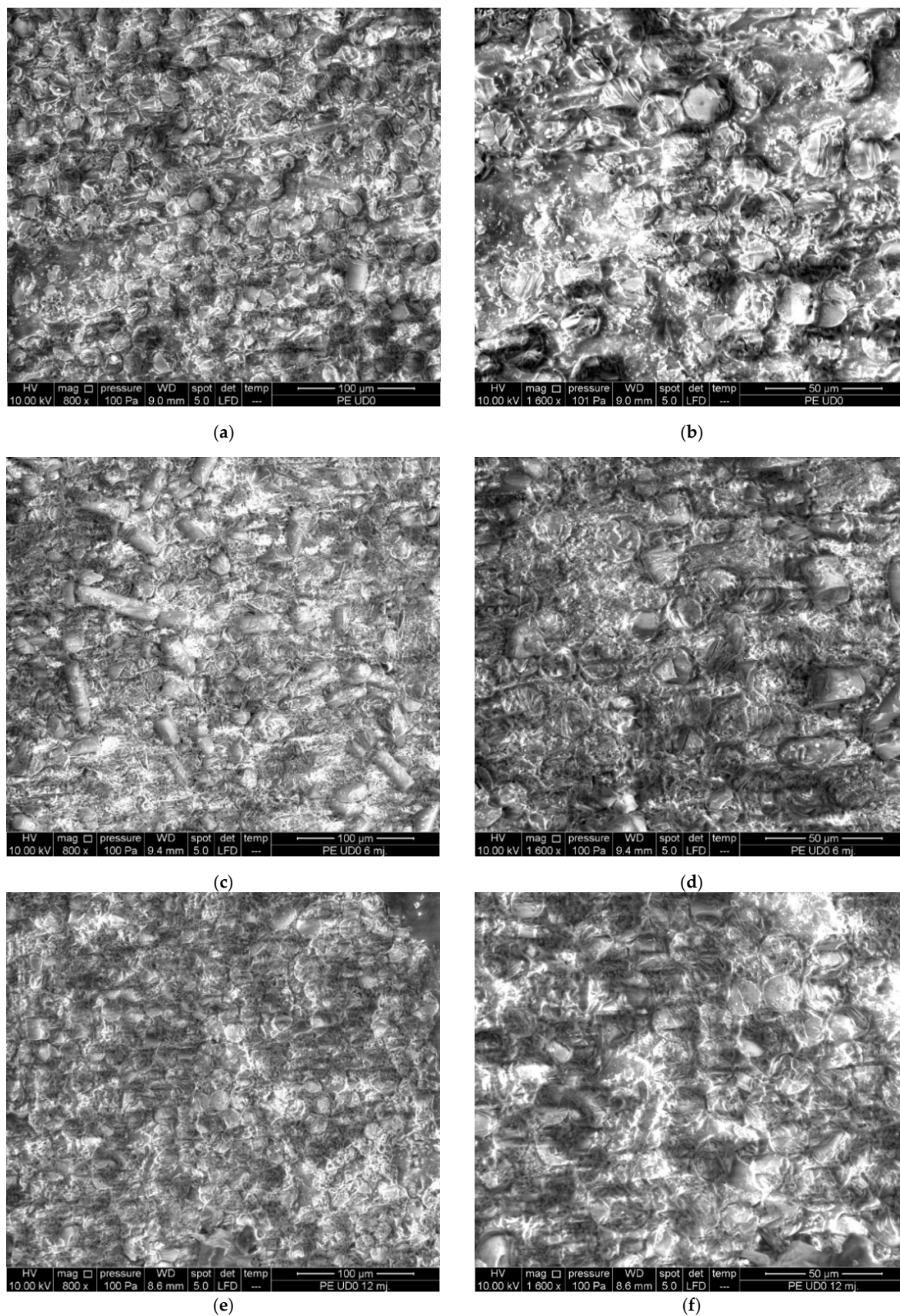


Figure 17. SEM polyester UD0^o: (a,b) dry; (c,d) salt crystals 6 months submersion; (e,f) 12 months submersion.

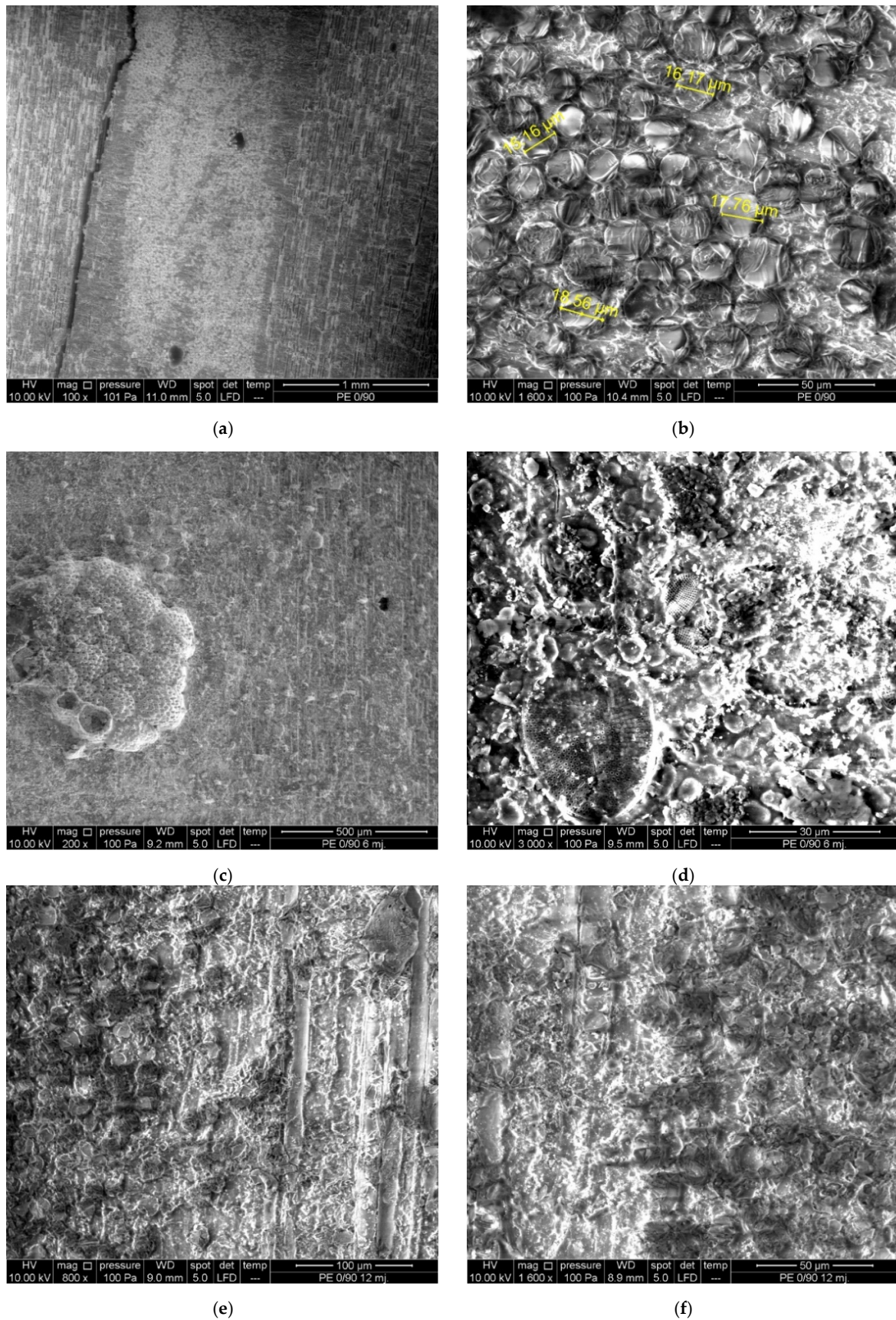


Figure 18. SEM polyester (0/90)s: (a,b) dry, manufacturing imperfections; (c,d) microorganisms' growth after 6 months of submersion; (e,f) 12 months of submersion.

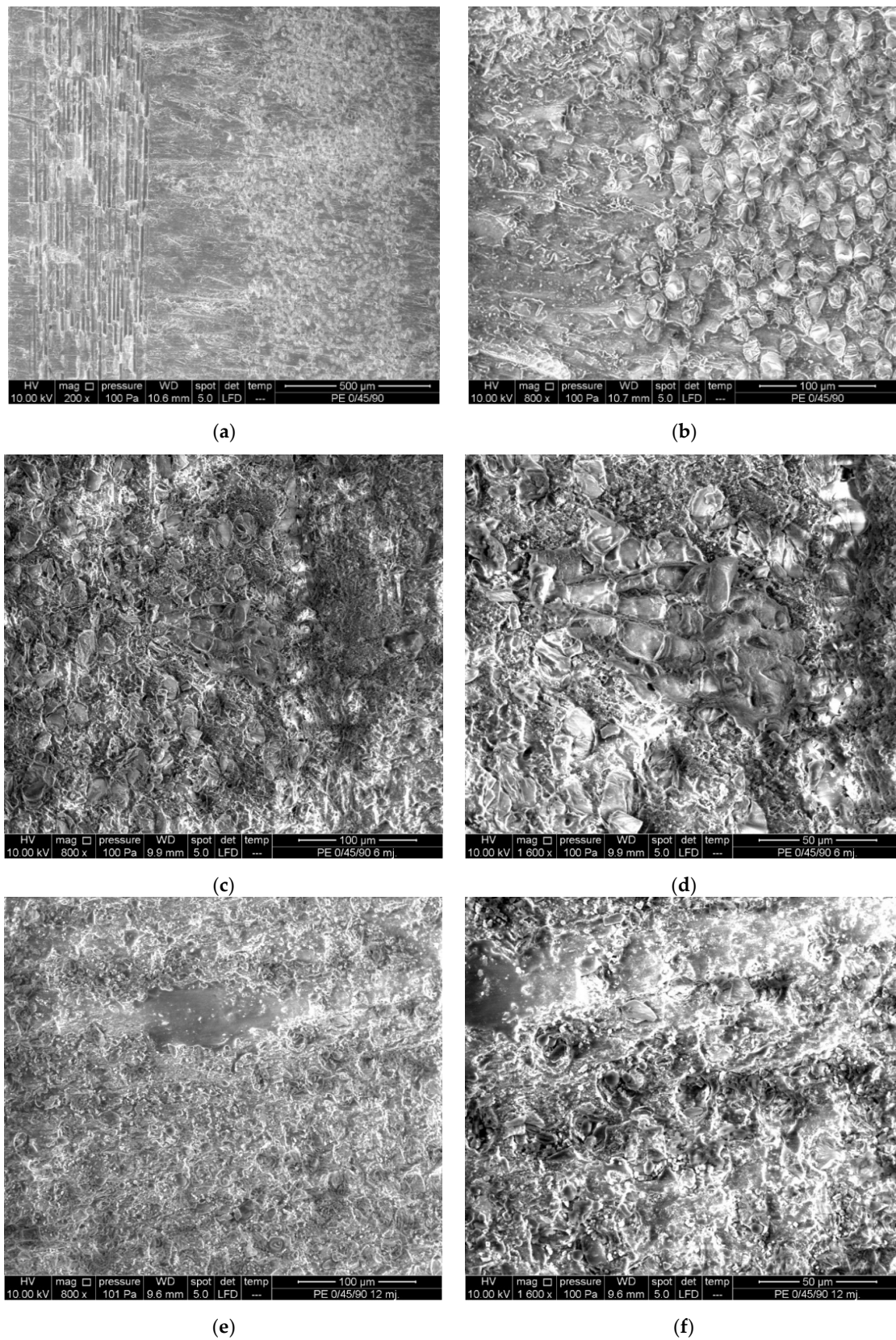


Figure 19. SEM polyester (0/45/90)s: (a,b) dry; (c,d) resin degradation, 6 months submersion; (e,f) microorganisms in the resin, 12 months of submersion.

4. Discussion

The mass measurement of all coupons before and after the submersion showed an increase of mass for all coupons, Tables 3 and 4, Figure 6. The epoxy resin coupons showed a greater average mass gain due to water absorption compared to polyester ones. Of the total of six resin material/fiber layout configurations, epoxy coupons with (0/90)s layout and all of the polyester coupons showed signs of water absorption saturation in the one year period. The epoxy UD0° and (0/45/90)s fiber layout have still and rising mass gain curve, indicating that water absorption saturation was not achieved after one year of submersion, Figure 6a. The (0/45/90)s fiber layout configuration coupons for both resin types showed the greatest mass gain compared to that of the other fiber layout configurations.

Polyester matrix coupons amassed more microbial growth than the epoxy ones. This emphasizes the importance of the application of real sea environment instead of, in similar research, more commonly used artificial sea and environmental conditions generated in a laboratory.

In all the diagrams in Figures 7–12, the reference stress-strain curve is designated as “Dry”. This curve represents the tensile mechanical properties of coupons not exposed to seawater. All submerged specimens had reduced tensile strength on average. Polyester resin coupons had a more pronounced drop in strength in the period from the 6th to the 12th month, Figure 13b, while the epoxy resin coupons exhibited greater tensile strength loss after the first 6 months of submersion. The only exception of this behavior was noticed in the epoxy coupons with the (0/90)s fiber layout configuration, Figure 14a. This is to be attributed to a single specimen from the group of this material and fiber layout combination submerged in the sea for 6 months exhibiting “extreme” tensile strength. By further examination, a higher fiber content in the said specimen was identified compared to that of the other specimens from the same group. This demonstrates that the manufacturing process has a strong impact on the mechanical properties of the finalized composite part.

Importantly, the environmental conditions (sea temperature, currents, sea level etc.) were not constant as they would be in a laboratory-based environment. The first 6 months of submersion spanned from late autumn to early summer i.e., predominantly colder environmental conditions. Subsequently, the next 6 months were predominantly warmer.

The results obtained in this research correlate with that of previous research by other researchers (pp. 129–142 in [5]) [37–39]. The novelty of this research is the exposure to real sea environment with all the environmental and sea living organisms’ effects acting simultaneously and randomly on the materials during the submersion, as opposed to, more commonly, artificial and laboratory conditions, often combined with accelerated absorption tests.

Analysis of the images collected during the microscopical investigation showed formation of salt crystals on the surface layers of the coupon as well as embedded salt crystals in both resins. The epoxy resin coupons showed a greater accumulation of salt crystals, Figures 14c, 15e and 16c, than polyester ones, Figures 17c, 18d and 19d, regardless of the fiber orientation setups.

One additional phenomenon noticed was the attachment and growth of marine microorganism on the organic resins used as matrix materials. The attachment and growth of sea microorganisms on the surface of the coupons was more intense in the first 6 months for the epoxy matrix coupons, but the total growth and maximum values after 12 months were more significant for the polyester ones, causing significant morphological changes in the resin, Figures 17e, 18d and 19f. The (0/45/90)s fiber configuration attracted the most microorganisms for the epoxy resin coupons, Figure 16e,f, while for the polyester ones, most organism were found in the (0/90)s configuration, Figure 18c,d. The algae attached to the surface of the coupons were easily removable during the cleaning of the coupons and did not leave any noticeable macroscopic damage areas on the coupons.

However, the microorganisms that settled on the coupon’s matrix were causing mechanical changes on the organic resin [40], effectively creating voids from the surface and

into the matrix; hence, additionally changing the mechanical properties of the composite. Since the polyester coupons were manufactured by hand layup, the number of imperfections and voids in the matrix was greater than in that of the vacuum-infused epoxy coupons. This resulted in a greater number of favorable locations for the development of microorganisms, and therefore, a greater influence on the mechanical properties of the composite material.

5. Conclusions

Considerable effects of the real sea environment on composite materials were noticed in the form of reduced mechanical strength for the tested coupons submerged in the sea. The submerged UD0, (0/90)s, and (0/45/90)s epoxy/glass coupons exhibited tensile strength reduction of 32%, 14%, and 36% after 6 months of submersion (with the exception of one inadequately manufactured (0/90)s coupon), whilst 44%, 40%, and 49% after 12 months of submersion, respectively. The polyester/glass UD0, (0/90)s, and (0/45/90)s coupons have lost 11%, 5%, and 1% after 6 months of submersion, and 50%, 37%, and 13% after 12 months in the sea. The (0/45/90)s layout configuration for the polyester/glass combination showed the greatest resilience to the marine environment. However, further study is needed here because the polyester coupons were made by hand-layup process, which can significantly affect mechanical characteristics of the composite. This issue will be examined more in detail when the currently submerged 24-month coupons batch is extracted from the sea.

The growth of microorganisms embedded in the resin and invertebrate (Nematoda) organism attached to the surface of the coupons effectively created voids in the matrix resin and produced a direct effect on mechanical properties. As microorganisms are only able to accelerate chemophysical erosion of the plastic surfaces in marine environment, probably through the secretion of corrosive substance (acids, hydrolytic catalyzers etc.), further in-depth research on this effect is necessary.

The findings of the research indicate the importance of biofouling in environmental degradation of mechanical properties of composite materials in the marine environment. Ageing of FRP composites in real-time and real marine environment differs with the more commonly used accelerated ageing methods due to the effects of the marine organisms attached to the material. This can affect the accuracy of results obtained by the artificial environment and accelerated testing methodology if sufficient care is not taken to assure the replication of real marine environment and its effects.

More data from longer exposure are needed to enable the development of a reliable predictive numerical model of the mechanical behavior of composite materials exposed to real sea environment, which would represent a basic tool to assess the durability and the sustainability of composite marine structures during their exploitation. Additional coupons were already submerged in the sea to ensure the continuation of this research. This additional set of data will help in building predictive numerical model that could successfully replace the time and resource consuming experiments. However, stochastic nature of the environmental loading must be incorporated in that model. For that reason, placing coupons in different types of marine environment (regarding the temperature, salinity, pH value, etc.) would bring even better accuracy of the numerical model. Also, when it comes to use of composites in marine industry, it would be beneficial to place the test coupons in different locations to account for change in the structure of micro-organisms due to ballast water discharge. This is the path that should be followed in future research.

Sustainability of composites in general in the marine industry was often emphasized in terms suggesting that composite materials offer the possibility of building lighter vessels that can carry more cargo and/or produce lower emissions, with the expansion of the maintenance intervals [41]. However, potential sustainability needs to be validated, since different types of composites react differently when exposed to harsh marine environment. This study presents a step in that direction giving insight into the behavior and change of

mechanical properties for specific type of composites exposed for prolonged periods to the real marine environment.

Supplementary Materials: The complete set of SEM images obtained during this research is available on Vizentin, Goran (2021), “Marine Composites SEM”, Mendeley Data, V1, doi:10.17632/j8tvmkpmwf.1.

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